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Joint Calibration of Multi-Platform Altimeter Measurements

of Wind Speed and Wave Height Over the Past 20 Years

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ABSTRACT

Since 1985 – for more than 23 years, seven altimeter missions have provided global coverage of significant wave height and wind speed. This study undertakes a long term analysis of the accuracy and stability of altimeter derived values of significant wave height and wind speed from the satellites: ERS1, ERS2, ENVISAT, GEOSAT, GEOSAT Follow-On (GFO), JASON1 and TOPEX. The study is a necessary step in developing a quality controlled and fully calibrated/validated dataset from the combined satellites. Calibration of all altimeters is performed against NODC buoy data over the extended period. These calibrations are validated using intercomparisons between satellite missions at cross-over ground points. This analysis shows that for a number of the satellites, small "step-like" changes occur during the missions. These inconsistencies are removed by sub-dividing these missions and undertaking a partial calibration for each section of the mission. The analysis also highlights that care is necessary when attempting to apply relationships between radar cross-section and wind speed derived for one altimeter to other platforms. Before undertaking such steps it is first necessary to apply a platform specific radar cross-section offset to the data.

1 1. Introduction

² Many oceanographic applications require the compilation of long-term databases of accu-³ rate oceanic properties (in the present case, significant wave height H_s and wind speed U_{10}). ⁴ Historically, such wave climate data is gathered through the deployment of oceanographic ⁵ buoys and more recently though the use of numerical models (Caires et al. 2004). Both ⁶ approaches have significant deficiencies. In situ buoy data has obvious limitations in terms

of geographical and temporal coverage and the expense of deploying and maintaining such 7 systems. Model data clearly solves these limitations, but relies critically on the accuracy 8 of the model. Even though present day models contain sophisticated representations of 9 wind-wave physics, the accuracy of such models is still limited (Tolman 2002). Studies 10 by e.g. Dobson et al. (1987) and Monaldo (1988) have shown that active remote sensing 11 satellites, particular Ku-band radar altimeter systems, are capable of measuring significant 12 wave height (H_s) and wind speed (U_{10}) to an accuracy comparable to in situ observations 13 (e.g. buoys). 14

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Since the launch of GEOSAT in 1985, a total of seven independent altimeter missions (cf. 2b) have been operational, potentially providing a unique database with global coverage spanning more than two decades. Once calibrated and quality controlled, such a database could be an invaluable tool for many oceanographic applications, such as:

• measurement of changes in global wind and wave climate

• development of methods to determinate extreme values

• investigation of extreme meteorological systems (i.e. hurricanes)

To date, however, these independent data sources have not been compiled to form one single, long term database. Although some attempts have been made to form datasets from combined altimeter missions (e.g. Cotton and Carter 1994; Callahan et al. 1994; Young 1999a; Alves and Young 2003), a comprehensive database of the type proposed has not previously been developed. Furthermore, procedures to process data gathered by polar orbiting altimeter satellites are still relatively underdeveloped. The future of oceanography will inextricably move towards satellite observations of the ocean, supported by in situ point
instruments for data calibration.

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This paper describes the development of such a database, including the validation, calibration and quality control of the data set. The arrangement of the paper is as follows. Section 2 describes both the buoy and altimeter data sources used. Section 3 provides details of the quality control and calibration/validation of the altimeter data. Calibrated results for wind speed and wave height are given within the subsections. Finally, the conclusions of the study are considered in Section 4 which provides a tabular summary of the final calibrated results for wind speed and wave height.

³⁹ 2. Data Sources

National Oceanographic Data Center (NODC) buoy data was used to provide in situ 40 data for a uniform calibration (ground truthing) for all altimeter missions over the entire 41 period (described below). The satellite data (Geophysical Data Records GDRs) were sourced 42 from the respective agencies and separately compiled for each available radar altimeter up to 43 2008, covering the historic satellite platforms GEOSAT, ERS1, and TOPEX and the ongoing 44 missions ENVISAT, ERS2, GFO, and JASON1. Note that the TOPEX/POSEIDON mission 45 included three separate altimeter instruments: TOPEX side A (cycles 1-235), side B (cycles 46 236–481), and the POSEIDON altimeter. The POSEIDON altimeter has not been considered 47 in this paper as its data is co-incident with TOPEX. 48

49 a. Buoy data

Wind and wave data were downloaded from the NOAA Marine Environmental Buoy Database, maintained by the NODC. The data archive contains records from various stations (e.g. lighthouses, oil platforms, and buoys, etc.) reporting a range of environmental parameters (e.g. air temperature, sea temperature, wind speed, wave height, wave direction, etc.) in constant time intervals (Evans et al. 2003). Despite the lack of spatial coverage this archive features an excellent temporal coverage back to the early seventies. For the present purposes, only moored buoys were processed.

<< Fig. 1, p. 40 (MapNODCBuoyLocation.eps) >>

The buoy data format (F291) contains nine different types of data records (e.g. nondirec-57 tional wave spectra, subsurface temperature/salinity, subsurface current, etc.). In the present 58 analysis, only header and environmental data records were processed [NODC (cited 2008)]. 59 In addition to geographic location and date/time, values of significant wave height, wind 60 speed, air/sea temperature, and anemometer height were extracted from the environmental 61 data records. The NODC moored buoy network consists of various platform types ranging 62 from 3 m, 6 m, 10 m, to 12 metre discus buoys (Meindl and Hamilton 1992). Large discus 63 buoys were deployed in areas of harsh climate, such as the Bering Sea and due to maintenance 64 services and refurbishing procedures, all buoys are subjected to changes in their location 65 with time (Meindl and Hamilton 1992). For calibration purposes the database consists of 66 195 different stations, distributed over 619 locations. The locations of the buoys are shown in 67 Figure 1, highlighting the restricted geographical distribution of data, with the vast majority 68

⁶⁹ of the locations being near continental North America and almost exclusively confined to⁷⁰ the Northern hemisphere.

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Each buoy type collects wind speed at a different height (anemometer height). Therefore a height based correction was applied to provide compatibility between buoy observations and altimeter estimated wind speeds at 10 metres (U_{10}) above the mean sea surface. Following Young (1999b) and assuming a logarithmic marine boundary layer, the records were corrected to 10 m reference height U_{10} using the relationship:

$$U_{10} = u \sqrt{\kappa^2 / C_d} \ln^{-1}(z/z_o)$$
 (1)

where u is the wind speed measured at a height z above sea level, z_o is the surface roughness 77 length, κ is the von Kármán constant and C_d the drag coefficient. The drag coefficient 78 varies with both wind speed and sea state (Young 1999b). However, field measurements of 79 C_d typically scatter over an order of magnitude. Noting this, and the inherent inaccuracies 80 associated with floating buoy measurements of wind speed (see later this section), a constant 81 value of C_d was used. For the present application, a representative value of $C_d = 1.5 \times 10^{-3}$ 82 was adopted and with the von Kármán constant $\kappa = 0.4$, (5.11) from Young (1999b) can 83 be solved to yield $z_o = 3.271 \times 10^{-4}$ m. This value of z_o is consistent with the relationship 84 developed by Donelan (1990) $z_o/H_{rms} = 5.53 \times 10^{-4} (U_{10}/C_p)^{2.66}$, where C_p is the phase 85 speed of the waves and H_{rms} is the root mean squared wave height. Typical open ocean 86 values of $U_{10}/C_p \approx 1$ and $H_{rms} \approx 0.8$ m yield results comparable to $z_o = 3.271 \times 10^{-4}$ m. 87

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⁸⁹ The buoy-network transmits hourly observations via the Geostationary Operational En-

vironmental Satellite (GOES) system to the data acquisition center (Hamilton 1986). Some 90 care needs to be exercised in interpreting the logging cycles for the buoys, which have changed 91 over the extended period being considered. Typically, the buoys record wind speed averaged 92 over a period of 8 minutes and the significant wave height from a time series of duration 93 20 minutes. On occasions, however, the significant wave height was determined from a 40 94 minute time series. The 20 minute wave records typically commence 20 minutes past the hour 95 and the wind records commence 42 minutes past the hour. On a small number of occasions, 96 the wave records commenced 30 minutes past the hour (i.e. both wind and wave records 97 conclude at 50 minutes past the hour). When 40 minute wave records were employed, these 98 records commenced on the hour. Records recorded after 5 May 1992, typically recorded the 99 observation time as 50 minutes past the hour (i.e. the time when wind and wave records 100 concluded). Prior to this date, the recording time was stored as the closest whole hour (i.e. 101 the next hour for records concluding at 50 minutes past the hour) (personal communication, 102 NODC). For the present analysis, the times associated with wind and wave records were 103 corrected to the centre of the respective time series. 104

In the present analysis, buoy data is used as the reference or "ground truth". However, 105 such data is not free of error, as it is limited by both sampling variability (i.e. the respective 106 time series are just one realisation of the process) (Bendat and Piersol 1971) and instrumental 107 accuracy. Floating buoys are subject to systematic bias. At low wind speeds, the rocking 108 motion of the buoy will "pump" the anemometer resulting in an overestimation of wind 109 speed. Conversely, at high wind speed/wave height, sheltering by wave crests will result in 110 an underestimation of the wind speed. Buoy accuracies are specified as 1.0 m s^{-1} for wind 111 speed and 0.2 m for significant wave height [NDBC (cited 2008)]. 112

113 b. Altimeter Data

Spaceborne Radar altimeters have observed the oceans for more than two decades. Figure 114 2 shows the various missions over this period. As can be seen, there is an almost continuous 115 record since 1985. The Radar altimeter can be used to estimate several oceanographic 116 parameters over a footprint ranging between 1 and 10 km in diameter (Chelton et al. 2001). 117 The precise size of a pulse-limited footprint depends on range, pulse width, and wave height 118 itself (Chelton et al. 2001). The footprint for GEOSAT is approximately 5 km (Cheney et al. 119 1987), ERS1, ERS2 and ENVISAT are 7 km, TOPEX, JASON1 are 6 km (Queffeulou 2004) 120 and GFO is approximately 3 km (Walker 1995). 121

<< Fig. 2, p. 41 (FigTemporalCoverageAlti.eps) >>

The altimeter estimates significant wave height (H_s) from the sea surface variance (σ^2) 122 which is characterized by the slope of the leading edge of the returned waveform (Chelton 123 et al. 2001; Holthuijsen 2007). The significant wave height is defined as $H_s = 4\sqrt{\sigma^2}$, where 124 σ^2 is the variance of the sea surface elevation (Chelton et al. 2001). Wind speed (U₁₀) is 125 related to the backscatter coefficient (σ_o) representing the ratio of the power scattered back 126 to the altimeter from the illuminated surface to the incident power (Chelton et al. 2001). For 127 small incident angles the radar cross-section, σ_o , can be inversely related to the surface wind 128 speed (Brown et al. 1981; Goldhirsh and Dobson 1985; Chelton and Wentz 1986; Witter and 129 Chelton 1991; Young 1993; Freilich and Challenor 1994; Young and Holland 1996; Chelton 130 et al. 2001; Abdalla 2007). Typically, altimeter measurements of H_s have smaller error than 131 for U_{10} when compared with buoy measurements and the accuracy (rms error) has been 132

stated as within 0.5 m for H_s and 1.8-2.0 m s⁻¹ for U_{10} . For TOPEX altimeter measurements, Kshatriya et al. (2001) state smaller values of 0.3 m and 1.6 m s⁻¹, respectively.

Data for each of the seven satellites was obtained, as detailed in Table 1. The details of the orbit geometry (i.e. repeat cycle and inclination angle) is different for each satellite. All systems were, however, placed in polar orbits providing global coverage, the period of data available being shown in Figure 2. As indicated in the table, in each case Geophysical Data Records (GDRs) have been used for the analysis. This is important as calibration values and data quality often varies between different altimeter data products.

<< Table 1 (p. 33) >>

¹⁴² 3. Quality Control and Validation/Calibration Methods

¹⁴³ a. Altimeter Quality Control

Geophysical Data Records (GDRs) are not free from errors and a visual examination of such data clearly shows data "spikes" (see Figure 3). Such erroneous data often occurs at the land/sea boundary, in the proximity of islands or over sea ice. In compiling a large database it is important that such erroneous data is removed in a reliable fashion, whilst not discarding reliable data. In a similar fashion to that proposed by Young and Holland (1996), a three-pass quality control process was applied to the data. 150 PASS 1

The GDRs contain data which enables an initial quality assessment. The first pass 151 focussed on the H_s data and flagged data which met any of the following criteria as erroneous: 152 • If $H_s > 30$ m the data point was flagged as erroneous. 153 • Most data sets contain a flag which indicates whether the data point is over ocean or 154 land/ice, based on a land/sea mask. All points identified as over land/ice were flagged 155 as erroneous. 156 • GDRs typically provide an observation approximately once per second. Each one 157 second value is the average of between 10 and 20 waveforms, depending on the satellite. 158 Waveforms which do not meet pre-defined parameters are discarded. If the final 159 number of waveforms averaged falls significantly below the maximum possible (10 or 160 20), then this is an indication that the data is of questionable quality. The number 161 of waveforms averaged for each point is typically recorded within the GDR. If the 162 number of averaged waveforms was less than $75\,\%$ of the maximum number, the data 163 was flagged as erroneous. 164

165 PASS 2

The data from Pass 1 was divided into blocks of 25 points. Such blocks represent approximately 180km along the ground track. This distance was considered large enough to obtain a representative group of observations (25 in this case), but not so long that there would be significant variability within the block due to geophysical processes (different wind ¹⁷⁰ systems etc.). A number of different block sizes were tested before adopting this value.

• Individual values in the block were flagged as erroneous if $\frac{|H_s - \bar{H}_s(block)|}{\sigma_{H_s}(block)} > 2$ where $\bar{H}_s(block)$ is the mean of the points in the block and $\sigma_{H_s}(block)$ is the standard deviation of the block.

174 PASS 3

In the final pass, blocks identified in Pass 2 were further considered. These blocks were re-divided into sub-blocks, either side of flagged points. These sub-blocks were further considered.

• each sub-block was examined for outliers, as in Pass 2, with any further points failing the test flagged as erroneous.

• If the ratio $R = \frac{\sigma_{H_s}(block)}{H_s(block)}$ is large, then it indicates that it is possible that there are multiple "spikes" in the block. Therefore, if R > 0.5 the entire sub-block was discarded.

$$<<$$
 Fig. 3, p. 42 (MapGFODespike.eps) $>>$

Figure 3 shows an example of a typical satellite pass with the raw GDR data (gray) and the quality controlled data (solid lines) shown. The ascending ground track is shown as a smooth line (left panel) with recorded wave height (H_s) and wind speed (U_{10}) along the ground track as a function of latitude (right panel). The most southern section of the track passes over the Antarctic continent towards the Southern Ocean. Due to the Southern Hemisphere Winter erroneous data below 60° S can be linked to sea ice. At approximately

30°S data "spikes" occur due to the transition from water to the Australian continent, 188 whilst the effects of islands are shown between 20° S and 10° N when the satellite passes 189 over Indonesia. Further north, valid data is shown, as the satellite passes over a typhoon in 190 the Philippine Sea (30° N) measuring wave heights of 9 m and wind speeds up to 20 m s⁻¹. 191 As the track continues (40° N) , it passes over the Kamtschatka Peninsula and finally enters 192 open waters moving towards the Arctic Ocean. As shown in this figure, the quality assurance 193 algorithm successfully flags erroneous data whilst not discarding quality observations, even 194 in areas where there are strong spatial gradients of wind speed and/or wave height. 195

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Over the full duration of each of the satellite mission, the quality control procedure removed inappropriate data records amounting to: 15.5% for GEOSAT, 9.6% for ERS1, 8.1% for ERS2, 4.7% for TOPEX, 9.0% for GFO, 8.4% for JASON1, and 17.1% for ENVISAT.

201 b. Altimeter Calibration

²⁰² Calibration of the altimeter data was carried out by comparing buoy measurements with ²⁰³ quasi-simultaneous radar observations for both significant wave height (H_s) and wind speed ²⁰⁴ (U_{10}) . In the case of altimeter wind speed a single wind speed model relating wind speed ²⁰⁵ to radar cross-section (σ_o) , applicable to all altimeter platforms was determined (see below, ²⁰⁶ this section). Comparisons between buoy and satellite altimeter data require criteria for ²⁰⁷ the spatial and temporal separation between such observations to be adopted. Following ²⁰⁸ Dobson et al. (1987); Monaldo (1988); Gower (1996); Queffeulou (2003, 2004); Queffeulou et al. (2004) these limits were set at 50 km and 30 min respectively. Since buoy data was largely reported hourly (Hamilton 1986), the largest temporal separation is 30 min, and following Monaldo (1988) such a time separation leads to an expected uncertainty of 0.5 m s⁻¹ for wind speed and 0.3 m for significant wave height.

213

Along-track averages were calculated for all matching transects (maximum 100 km, i.e. 214 ± 50 km, assuming there is no land over the 100 km) and time tags of each altimeter overpass 215 were linear interpolated to the two nearest hourly buoy records for H_s and U_{10} respectively. 216 The 50 km spatial separation criteria defines a circle of diameter 100 km in which data is 217 considered. A transect which passes directly over the buoy will have a transect length of 218 100 km. More distant passes will define shorter chords of the circle. Only transects with 219 greater than 4 valid points were considered, so as to ensure statistically stable values. In 220 order to ensure that the point buoy measurements and the spatially averaged altimeter data 221 are comparable, it is desirable not to consider data recorded close to land, where there may 222 be strong spatial gradients of wave height or wind speed. Therefore, buoy stations within 223 40 km of land were not considered in the calibration process (Dobson et al. 1987). 224

225

Dobson et al. (1987) and Monaldo (1988) analysed typical errors associated with altimeter-buoy comparisons, considering spatial and temporal separation, buoy record duration and altimeter footprint averaging size, as well as platform-specific instrumental error. Monaldo concluded that differences for H_s and U_{10} of approximately 0.4 m and 1.8 m s⁻¹ respectively, can be expected, when comparing altimeter and buoy estimates, whereas Dobson et al. determined that an overall rms uncertainty for H_s and U_{10} of 0.5 m and 1.8 m s⁻¹, respectively, may be expected using collocated measurements within a 50 km range.

233

Collocated buoy-altimeter measurements were compared using linear regression analysis. 234 Since both variables (buoy and altimeter) have measurement uncertainty associated with 235 them, a traditional regression analysis is not appropriate (Stoffelen 1998). Rather, a reduced 236 major axis regression (RMA) was used to estimate the best-fit between the two measurements 237 (Trauth 2007). RMA regression is applicable when errors in both quantities need to be 238 considered. The RMA methodology minimizes the triangular area between the data point 239 and the regression line (Trauth 2007). Mayor outliers were eliminated prior to application 240 of the RMA analysis. This was achieved by applying a robust regression algorithm and 241 eliminating data points with low weighting. Robust regression is an iteratively re-weighted 242 least squares analysis (O'Leary 1990). 243

<< Fig. 4, p. 43 (FigScatterEnvisatBuoy.eps) >>

Figure 4 illustrates a typical calibration result, for JASON1 altimeter data. Clearly observable is the significantly higher scatter for U_{10} than for H_s . Note, that scatter plots for all other satellites look similar and therefore are not shown. The resulting RMA analyses for all satellites are however given in Table 3.

248

To evaluate the suitability of the final regression analysis, the following statistical parameters were evaluated: root mean square error, RMSE (Eq. 2), mean absolute error, MAE(Eq. 3), Pearson's correlation coefficient, ρ (Eq. 4), the number of sample points and the ²⁵² number of outliers.

$$RMSE: \ \epsilon = \sqrt{\frac{1}{n} \sum^{n} (\hat{y} - y)^2}$$
⁽²⁾

$$MAE: e = \frac{1}{n} \sum_{n=1}^{n} |\hat{y} - y|$$
(3)

$$\rho(Y, \hat{Y}) = \frac{Cov(Y, Y)}{\sqrt{Cov(Y, Y)Cov(\hat{Y}, \hat{Y})}}$$
(4)

In Equations (2)-(4), the hat separates the estimate (calibrated value) from the reference measurement (buoy observation) and Cov is the covariance between two random variables. The values of y take on either H_s or U_{10} and the upper case values refer to vectors.

256

Although the RMA analysis can be performed directly for values of H_s , its application 257 for U_{10} firstly requires the adoption of an appropriate wind speed algorithm relating U_{10} 258 and the radar cross-section, σ_o . A wide range of such wind speed algorithms have been 259 published. In general one can distinguish between one- and two-parameter wind speed 260 models (Fig. 5). Amongst others, Monaldo and Dobson (1989) and Gourrion et al. (2002) 261 investigated the enhancement of wind speed estimates by adding significant wave height as 262 an additional parameter in the wind speed function. A comprehensive summary of wind 263 speed algorithms (incl. equations) can be found in Young (1993) and Young and Holland 264 (1996). In this analysis, all major wind speed algorithms including: Brown et al. (1981); 265 Chelton and McCabe (1985); Chelton and Wentz (1986); Goldhirsh and Dobson (1985); 266 Witter and Chelton (1991); Freilich and Challenor (1994); as well as the recent models from 267 Gourrion et al. (2002) and Abdalla (2007) were compared with NODC buoy measurements, 268 and validated for performance using RMS error estimates from Eq. (2). Published wind speed 269 algorithms were typically derived for one particular altimeter platform (e.g. for SEASAT as 270

in Chelton and McCabe 1985), thus the possibility of a platform related bias (c.f. Table 2) 271 has to be considered before applying a uniform wind speed model to the data from multiple 272 altimeter missions. With the present data set, it would be possible to develop and fit an optimal functional form to the combined data set of $U_{10} - \sigma_o$ values. As the many existing 274 functions are, however, very similar, as shown in Figure 5, such a process was not attempted. 275 Comparisons with available data did, however, show that there were clear σ_o offsets between 276 the data sets and when applying an algorithm to a satellite for which it was not derived, 277 the offset needs to be considered. The rms error (ϵ) between the wind speed model and in 278 situ buoy measurements was minimized by selecting the optimal offset for the radar cross 279 section σ_o . The resulting values are shown in Table 2. These offset values need to firstly 280 be applied before a specific algorithm can be applied to a specific satellite data set. It is 281 clear that the bulk of the available data in Figure 5 is concentrated between 4 m s⁻¹ and 10 282 m s⁻¹. In order to ensure the algorithm fit is not biased to this region, data was averaged 283 into 5 cm $\rm s^{-1}$ bins and these average values used in the optimization. 284

$$<<$$
 Table 2 (p. 34) >>

It remains unclear if sea-state dependence, particular significant wave height (H_s) , should be considered. Although this was the subject of previous research, e.g. Monaldo and Dobson (1989); Glazman and Greysukh (1993) and Gourrion et al. (2002), results differ. As stated by Monaldo and Dobson, significant wave height potentially affects the physical link between σ_o and surface wind speed in two ways. First, the local wave heights are the combination of waves which propagate into the area and wind waves generated by local wind fields. Second, the presence of waves may affect the development of short waves on the surface, which influence the radar cross-section. Distinguishing such affects within the scatter of the data is challenging, as seen in Figure 5. The error analysis in Table 2 shows no clear reduction in RMS error with the inclusion of H_s as an additional parameter. For these reasons, two-parameter functions involving H_s have not been considered further in this analysis.

<< Fig. 5, p. 44 (FigTopexWindSpeedAlg.eps) >>

Based on error statistics from Eq. (2) to (4) the model proposed by Abdalla (2007) 296 was selected as the default wind speed algorithm for the database and is briefly described 297 below. Abdalla investigated the relationship between surface wind speed, as obtained from 298 the numerical wind model of the European Centre for Medium-Range Weather Forecasting 299 (ECMWF) and Ku-band altimeter backscatter coefficients from ENVISAT. The resulting 300 algorithm was derived from two months (January – February 2005) of collocation data 301 containing approximately 163,000 samples. Finally, the algorithm was verified against model 302 wind speed for ENVISAT (two years), JASON1 (18 months), and ERS2 (five years) altimeter 303 measurements. Abdalla adopted a two branch approach to estimate a first-guess wind speed 304 (U_m) by fitting linear and exponential segments for lower and higher radar cross section (σ_o) 305 respectively (cf. Eq. (5)). 306

$$U_m = \begin{cases} 46.5 - 3.6 \cdot \sigma_o & \text{for } \sigma_o \le 10.917 \text{ dB} \\ 1690 \cdot exp(-0.5 \cdot \sigma_o) & \text{for } \sigma_o > 10.917 \text{ dB} \end{cases}$$
(5)

³⁰⁷ Fine-tuning was carried out to ensure that model wind speeds matched buoy observations,

with U_m from Eq. (5) adjusted to:

$$U_{10} = U_m + 1.4 \cdot U_m^{0.096} \cdot exp(-0.32 \cdot U_m^{0.096}) \tag{6}$$

In Eq. (5) and (6) wind speed values have units of $[m s^{-1}]$ and Radar cross-section has units of [dB]. Since 24 October 2005, equations (5) and (6) have been used operationally for the ENVISAT radar altimeter (Abdalla 2007).

312

As the Abdalla (2007) relationship was derived for data with $U_{10} < 18 \text{ m s}^{-1}$, a modified form of the Young (1993) high wind speed relationship was adopted for $U_{10} > 18 \text{ m s}^{-1}$. The offset in Eq. (7) was modified, such that it intercepts the Abdalla (2007) result at 18 m s^{-1} .

$$U_{10} = -6.4 \cdot \sigma_o + 69$$
, if Eq. (6) > 18 m s⁻¹ (7)

In Eq. (7) U_{10} has units of $[m \ s^{-1}]$ and σ_o has units of [dB]. Although the error statistics supported the adoption of the Abdalla (2007) algorithm as the preferred wind speed model, a visual inspection of Table 2 shows that the widely applied Witter and Chelton (1991) algorithm also performs well.

320

With an appropriate wind speed algorithm adopted, it is possible to carry out the calibrations of both H_s and U_{10} for each of the altimeters. Table 3 provides the RMA derived calibration results for each of satellites. The results shown represent the average over the entire period of operation for each satellite mission and utilize all co-located buoy observations over that period. In addition, a subset of published altimeter calibration models is also shown for comparison purposes.

$$<<$$
 Table 3 (p. 35) >>

³²⁷ Queffeulou (2003) adopted a very similar calibration approach (averaging altimeter tran-³²⁸ sect within 50 km radius and 30 min temporal separation) to that proposed here, but based ³²⁹ on a shorter database. As can be seen from Table 3 the present results are in good agreement ³³⁰ with Queffeulou (2003) for H_s across all satellite missions. Young (1999a) used a database of ³³¹ 10 years duration, but compared monthly means within 4° by 4° bins, rather than co-located ³³² passes. This different methodology appears to give rise to measurable differences in the ³³³ calibration results.

334

For GEOSAT H_s , Dobson et al. (1987) proposed that the altimeter is generally 0.40 m lower than buoy observations ($\epsilon = 0.49$ m, e = 0.36 m and n = 116). Carter et al. (1992) provided evidence for a GEOSAT scaling error with altimeter values being 13% lower than buoy values. However, ordinary least square regression, not forced through the origin, leads to $H_s^* = 1.093 H_s + 0.116$ (n = 164), where H_s^* is the corrected significant wave height (Carter et al. (1992)), which is in good agreement with the result presented here.

341

Ray and Beckley (2003) correlated TOPEX and JASON1 significant wave height with buoy observations and concluded that for TOPEX, $H_s^* = 1.046 H_s - 0.070$ ($\epsilon = 0.17$ m, $\rho = 0.985$ and n = 399) and for JASON1, $H_s^* = 1.100 H_s - 0.104$ ($\epsilon = 0.21$ m, $\rho = 0.983$ and n = 368). The TOPEX result is in excellent agreement with the present result, which uses approximately ten times the amount of data. The JASON1 result differs slightly from the ³⁴⁷ present result with a larger slope but more negative offset.

348

For wind speed, it is not possible to directly compare the results with previous calibrations. In the present analysis, the Abdalla (2007) wind speed algorithm was adopted for all satellites, but with a σ_o offset for each satellite chosen so as to reduce the RMS error. The resulting values of altimeter wind speed were then further calibrated against co-located buoy wind speed using the RMA analysis. Not surprisingly, the results all have regression slopes near 1.00 and small offsets.

355 c. Altimeter Collocation Analysis

For much of the period under consideration (since 1993), multiple altimeter missions have 356 been in orbit. As a result, it is possible to cross-validate instrument performance against 357 other platforms, by comparing observations at cross-over points. Ground-track crossovers 358 between simultaneously operating altimeter platforms were considered when both platforms 359 passed the same ground point within 30 min. In contrast to Queffeulou (2004), 100 km (50 km 360 each side) along-track averages were compared, rather than the closest 1-s measurements. As 361 for the buoy comparisons, the spatial average provides a more statistically stable comparison 362 than a single point observation. For all platforms, a valid ground-track contains at least ten 363 individual 1-s altimeter data points for averaging. The altimeter cross-over analysis was not 364 used to calibrate individual platforms, this process being undertaken with the buoy analysis 365 (cf. Section 3b). Rather, scatter plots comparing different altimeters at cross-over points 366 were used as independent validation of the calibrated results. In other words, the cross-over 367

analysis was used as a quality control and validation measure.

<< Fig. 6, p. 45 (MapEnvisatERS2Collocation.eps) >>

Figure 6 shows an example of the spatial coverage of cross-over points for the overlap period of JASON1 and ERS2. In comparison to the buoy calibration process, the very much larger number of co-locations is clear. Figure 7 shows the resulting wave height and wind speed scatter plots for this same case. For all combinations of coincident satellite missions, the calibrated satellite altimeters produced consistent results (RMA regression slope close to 1:1), when averaged over the full durations of co-incident operation.

<< Fig. 7, p. 46 (FigScatterEnvisatERS2.eps) >>

375 d. Long Term Monitoring

The calibrations performed against buoy data (Table 3) considered all available data 376 for the period of operation of each satellite. As a result, the calibrations are averages over 377 the full satellite missions. It is important to ensure that the calibrations do not vary over 378 the duration of the extended mission. This could be determined by examining differences 379 between buoy and altimeter data as a function of time. A further possibility is to examine 380 differences between co-incident altimeter missions as a function of time at cross-over points. 381 Due to the very much larger data sets for altimeter cross-over points, this second option 382 proved more reliable, with a greater capability in identifying small changes in instrument 383 performance. 384

Figure 8 shows an example of the differences between TOPEX and ERS2 values of H_s . 385 Due to the large number of observations, data points shown in the plot were thinned using 386 block averages over n points (values of n are given in figure captions, e.g. 20/1 for a 387 20 point blocked average). If significant discontinuities or data drifts were determined, 388 the data sets were partitioned and a reduced major axis regression was applied for each 389 section of mission. For consistency, the partitioned RMA regression was performed against 390 buoy data, the cross-over analysis acting as an independent quality control. For wind 391 speed measurements, the previously determined, satellite specific, σ_o offsets were retained, 392 any further departures from buoy measurements be corrected using the partitioned RMA 393 analysis. Once the partitioned RMA analysis had been applied, the satellite cross-over plots 394 were examined to ensure the process had removed any inconsistencies between the data sets. 395

<< Fig. 8, p. 47 (FigTopexDrifCorrection.eps) >>

The most obvious example of a time-specific variation in altimeter performance is the TOPEX drift in H_s which commenced at approximately cycles 163–170 and continues to cycle 235 (April 1997 to January 1999), previously investigated by Challenor and Cotton (1999) and Queffeulou (2004). Challenor and Cotton applied a linear trend model to buoy measurements to remove the drift, whereas Queffeulou fitted a third order polynomial using ERS2 as the reference data set. As illustrated in Figure 8 the drift can be well approximated by an exponential power function of the form:

$$f(t) = 0.0542 \cdot \left[\exp(0.0027t)\right]^{1.1080} - 0.0303 \tag{8}$$

where the dependent variable t is time, measured in days from 25 April 1997 and f(t) has

units of [m]. The correction is valid until 30 January 1999 (0 days $\leq t < 645$ days). Figure 8 also shows the results once TOPEX data has been corrected using Eq. (8).

<< Fig. 9, p. 48 (FigTopexDrifCorrectionBuoys.eps) >>

Figure 9 shows the difference between TOPEX and buoy H_s , following the removal of the drift. In both cases, Eq. (8) successfully corrects the data. The reduction in available data in Figure 8 since June 2003, is a result of an onboard storage failure on ERS2, which has limited available data from this satellite to locations in the Northern Hemisphere close to receiving stations. This feature is also apparent in Fig. 6.

<< Fig. 10, p. 49 (FigERS1Discontinuities.eps) >>

Changes in altimeter calibration for either U_{10} or H_s were identified for ERS1, ERS2, 411 GFO and TOPEX using this process. Figure 10 shows differences between buoy and ERS1 412 H_s and U_{10} for the duration of the ERS1 mission. As explained above, changes to calibration 413 were actually identified using altimeter cross-over comparisons. The partial re-calibration 414 was then performed against buoy data and checked using cross-over comparisons. As no 415 single pair of altimeters covers the full ERS1 mission, the buoy comparison is used here for 416 illustrative purposes. The period between 1. January 1994 and 18. February 1995 clearly 417 shows slightly low values of H_s . To correct this effect, the full ERS1 mission was divided 418 into three sections and the partial RMA analysis applied to each section. The panels to the 419 right of Figure 10 show the corrected results, with the offset removed. 420

<< Fig. 11, p. 50 (FigGFODiscontinuities.eps) >>

Figure 11 shows a similar plot for GFO. Here, discontinuities in U_{10} in the periods before 21. December 2000 and after 21. January 2007 are clear. Again, the partial RMA analysis successfully accounted for these anomalies.

424

The source of these inconsistencies is unclear and may result from changes to onboard systems, different software implementations etc. Although the long term differences are relatively small (generally less than 1 m s⁻¹ in wind speed and 0.2 m in wave height), the value of a long term data base of this type requires confidence in the long term stability of the data.

430

In the case of TOPEX, the altimeter was changed from the Side-A instrument to Side-B in February 1999. The data did not show a measurable discontinuity at this point, nor any clear degradation in the quality of the Side-A data leading up to the change. This result is consistent with the Side-B calibration study reported by Dorandeu (1999).

435

The final calibrations for all satellites are provided in Table 4, which details the calibration results applicable in various periods for each satellite, as well as error statistics.

438 4. Conclusion

The data and procedures outlined here present a detailed analysis of the historic altimeter 439 data base of H_s and U_{10} over the more than 2 decades for which data is available. The 440 process developed calibrates the altimeter records against buoy data and then independently 441 validates these results against independent altimeter missions at cross-over points of ground 442 tracks. The value of such a data set is in that it covers an extremely long duration with 443 global coverage. As such, it is critical that altimeter calibration is stable over this extended 444 duration. This analysis investigates the long term stability of the altimeter missions and 445 concludes that long-term drift of results is generally not an issues (with the exception of 446 TOPEX H_s). However, a number of the missions do exhibit apparent step changes in 447 calibration at various times. Although these changes are not large, they do impact the overall 448 quality and reliability of the data set. These changes in calibration can, however, be corrected 449 by partitioning the data sets with time and independently calibrating the altimeter in each 450 partitioned segment. The reason for these step changes in calibration does not appear to 451 have been well documented and is presumably the result of changes in the software/hardware 452 of the satellite or of processing methods. 453

454

A number of relations between the radar cross section and wind speed were investigated and the Abdalla (2007) relationship was ultimately adopted for use with all altimeters. However, the analysis clearly shows that before applying such a relationship across all altimeters, a platform dependent offset must be applied.

459

Consistent with previous studies, altimeter values of H_s exhibit greater accuracy than U_{10} . Following calibration, the accuracy of the various altimeters are similar, with the rms error being less than 0.25 m for H_s and 1.7 m s⁻¹ for U_{10} .

463

In this study no attempt has been made to look at long-term trends in the final "calibrated" dataset. This is an involved task which requires a careful analysis of the data. The present dataset does, however, provide a unique resource for such studies and this is the subject of ongoing research.

<< Table 4 (p. 36) >>

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597		calibrations are shown.	36

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Source	CD-ROM							CD-ROM	CD-ROM	CD-ROM	Internet	Internet	Internet	
Format	CEOS	CEOS	CCSDS	CEOS	CEOS	CEOS	CCSD	CCSD	RA-2/MWR Level 2	JGM3-GDR	GDR	PODAAC IGDR and GDR	PODAAC MGDR-B	
Agency	ESA	ESA	ESA	ESA	ESA	ESA	ESA	ESA	ESA	NOAA	NOAA	NASA	NASA	
Inclination	98.54°							98.54°	98.54°	108.00°	108.04°	66.04°	66.04°	
Repeat Cycle	3 days	3 days	35 days	3 days	168 days	168 days	35 days	35 days	35 days	17 days	17 days	10 days	10 days	
Dates	10 December 1991	30 March 1992	20 December 1993	10 April 1994	26 September 1994	21 March 1995	17 May 1996	8 September 2008	17 November 2008	01 January 1990	01 July 2008	03 May 2008	08 October 2005	
	I	I	Ι	I	I	I	Ι	Ι	I	Ι	I	Ι	I	
	01 August 1991	28 December 1991	14 April 1992	23 December 1993	10 April 1994	28 September 1994	21 March 1995	21 April 1995	24 September 2002	30 March 1985	07 January 2000	15 January 2002	22 September 1992	
Satellite	ERS1							ERS2	ENVISAT	GEOSAT	GFO	JASON1	TOPEX	

TABLE 1. Summary of altimeter data products and characteristics including orbit parameters, name of data format and data source.

TABLE 2. Platform specific σ_o bias (i.e. the reported bias needs to be added to the satellite σ_o values) with related rms error ϵ for selected wind speed algorithms: Brown et al. (BR1981), Goldhirsh and Dobson (GD1985), Chelton and Wentz (CW1986), Witter and Chelton (WC1991), Freilich and Challenor (FC1994), Abdalla (A2007), and Gourrion et al. (GVC2002).

Altimeter	BR1981	GD1985	CW1986	WC1991	FC1994	A2007	GVC2002
ERS1	-0.205 dB	-0.264 dB	$+0.095\mathrm{dB}$	$-0.039\mathrm{dB}$	-0.177 dB	$+0.075\mathrm{dB}$	$+0.578\mathrm{dB}$
ϵ	$1.32{\rm m~s^{-1}}$	$1.23{\rm m~s^{-1}}$	$1.41{\rm m~s^{-1}}$	$1.20{\rm m~s^{-1}}$	$1.26{\rm m~s^{-1}}$	$1.14 { m m s^{-1}}$	$1.18{\rm m~s^{-1}}$
ERS2	$-0.154\mathrm{dB}$	$-0.241\mathrm{dB}$	$+0.093\mathrm{dB}$	$-0.045\mathrm{dB}$	$-0.209\mathrm{dB}$	$+0.075\mathrm{dB}$	$+0.512\mathrm{dB}$
ϵ	$1.32{\rm m~s^{-1}}$	$1.27{\rm m~s^{-1}}$	$1.62{\rm m~s^{-1}}$	$1.34{\rm m~s^{-1}}$	$1.45{\rm m~s^{-1}}$	$1.25{ m m~s^{-1}}$	$1.29{\rm m~s^{-1}}$
ENVISAT	$-0.363\mathrm{dB}$	$-0.431\mathrm{dB}$	$-0.114\mathrm{dB}$	$-0.268\mathrm{dB}$	$-0.424\mathrm{dB}$	$-0.138\mathrm{dB}$	$+0.299\mathrm{dB}$
ϵ	$1.31{\rm m~s^{-1}}$	$1.26{\rm m~s^{-1}}$	$1.56{ m m~s^{-1}}$	$1.33{\rm m~s^{-1}}$	$1.39{\rm m~s^{-1}}$	$1.21{ m m~s^{-1}}$	$1.27{ m m~s^{-1}}$
GEOSAT	$-0.060\mathrm{dB}$	$-0.053\mathrm{dB}$	$+0.160\mathrm{dB}$	$+0.087\mathrm{dB}$	$-0.073\mathrm{dB}$	$+0.225\mathrm{dB}$	$+0.595\mathrm{dB}$
ϵ	$1.71{\rm m~s^{-1}}$	$1.68{\rm m~s^{-1}}$	$1.96{\rm m~s^{-1}}$	$1.80{\rm m~s^{-1}}$	$1.91{\rm m~s^{-1}}$	$1.75{ m m~s^{-1}}$	$1.98{\rm m~s^{-1}}$
GFO	$-0.731\mathrm{dB}$	$-0.796\mathrm{dB}$	$-0.433\mathrm{dB}$	$-0.595\mathrm{dB}$	$-0.755\mathrm{dB}$	$-0.481\mathrm{dB}$	$-0.031\mathrm{dB}$
ϵ	$1.37{\rm m~s^{-1}}$	$1.32{\rm m~s^{-1}}$	$1.64{ m m~s^{-1}}$	$1.39{\rm m~s^{-1}}$	$1.47{\rm m~s^{-1}}$	$1.28 \mathrm{m} \mathrm{s}^{-1}$	$1.36{\rm m~s^{-1}}$
JASON1	$-1.036\mathrm{dB}$	$-1.115\mathrm{dB}$	$-0.779\mathrm{dB}$	$-0.939\mathrm{dB}$	$-1.056\mathrm{dB}$	$-0.789\mathrm{dB}$	$-0.361\mathrm{dB}$
ϵ	$1.38{\rm m~s^{-1}}$	$1.36{\rm m~s^{-1}}$	$1.72{ m m~s^{-1}}$	$1.44{\rm m~s^{-1}}$	$1.54{\rm m~s^{-1}}$	$1.33{ m m~s^{-1}}$	$1.36{\rm m~s^{-1}}$
TOPEX	$-0.752\mathrm{dB}$	$-0.837\mathrm{dB}$	$-0.469\mathrm{dB}$	$-0.627\mathrm{dB}$	$-0.777\mathrm{dB}$	$-0.502\mathrm{dB}$	$-0.108\mathrm{dB}$
ϵ	$1.27{\rm m~s^{-1}}$	$1.21{\rm m~s^{-1}}$	$1.49{\rm m~s^{-1}}$	$1.21{\rm m~s^{-1}}$	$1.32{\rm m~s^{-1}}$	$1.14 \mathrm{m} \mathrm{s}^{-1}$	$1.16{ m m~s^{-1}}$

TABLE 3. Overall calibration results using reduced major axis (RMA) regression. The analysis uses all available buoy-altimeter co-locations (n) for the full period of each altimeter mission. Also shown are results from earlier studies. Altimeter wind speed U_{10} was calculated from the Abdalla (2007) model and platform specific biases were applied (cf. Table 2).

								Queff	eulou et a	1. (2004) for I	I_s			
			Zieg	ger, Vinoth and	d Young (2009			Queff	eulou (200	(3) for U_{10}		You	ng (1999a)	~
	Altimeter	slope	offset	e	e	β	n	slope	offset	e	u	slope	offset	u
	ENVISAT	1.069	-0.198	$0.15\mathrm{m}$	$0.12\mathrm{m}$	0.990	4390	1.033	-0.183	$0.19\mathrm{m}$	1,280			
	ERS1	1.127	+0.280	$0.20\mathrm{m}$	$0.16\mathrm{m}$	0.984	2079					1.243	+0.040	192
:	ERS2	1.076	+0.042	$0.17\mathrm{m}$	$0.13\mathrm{m}$	0.989	7885	1.064	+0.001	$0.19\mathrm{m}$	12,070			
^{s}H	GEOSAT	1.076	+0.122	$0.21\mathrm{m}$	$0.17\mathrm{m}$	0.982	1600					1.144	-0.148	203
	GFO	1.068	+0.102	$0.15\mathrm{m}$	$0.12\mathrm{m}$	0.991	6179	1.080	+0.039		21,228			
	JASON1	1.036	+0.026	$0.16\mathrm{m}$	$0.13\mathrm{m}$	0.990	4420	1.007	+0.039	$0.19\mathrm{m}$	2,853			
	TOPEX	1.049	-0.098	$0.17\mathrm{m}$	$0.13\mathrm{m}$	0.990	3428	1.024	-0.048	$0.17\mathrm{m}$	7,826	1.067	-0.079	192
	ENVISAT	1.010	-0.110	$1.11{ m m~s^{-1}}$	$0.86{ m m~s^{-1}}$	0.941	2926	0.964	+0.599	$1.52{ m m~s^{-1}}$	292			
(20	ERS1	1.047	-0.293	$1.07{ m m~s^{-1}}$	$0.83{ m m~s^{-1}}$	0.984	1333					0.849	+1.217	192
007	ERS2	1.005	-0.024	$1.20{ m m~s^{-1}}$	$0.93{ m m~s^{-1}}$	0.931	5093							
;¥)	GEOSAT	1.015	-0.087	$1.76{ m m~s^{-1}}$	$1.31\mathrm{m~s^{-1}}$	0.857	1113					0.874	+0.337	196
0	GFO	0.986	-0.059	$1.31{ m m~s^{-1}}$	$1.02{ m m~s^{-1}}$	0.925	4136							
Ω	JASON1	0.999	+0.070	$1.28{ m m~s^{-1}}$	$0.99{ m m~s^{-1}}$	0.936	2865	0.986	+0.887	$0.85{ m m~s^{-1}}$	1,236			
	TOPEX	1.010	-0.062	$1.11{ m m~s^{-1}}$	$0.87{ m m~s^{-1}}$	0.948	2486					0.943	+1.847	190

TABLE 4. Calibration results for all altimeters and periods over which the calibration is valid. Results are shown for both significant wave height (H_s) and 10 m wind speed (U_{10}) , where the asterisk indicates the corrected value. Error statistics, rms error (ϵ) , mean absolute error (e), correlation coefficient (ρ) , the number of samples (n), rate of outliers, and the number of buoy stations used for the calibrations are shown.

Bouys	87	58	58	58	87	42	78	60	45	87	58	58	58	87	87	87	87	42	78	78	78	60	45	45	45
Outlier	2.6%	1.7~%	1.0%	2.2%	2.2~%	2.3%	2.9%	2.8%	2.5%	1.8%	1.7~%	2.1%	1.3%	2.1%	0.0%	1.7~%	1.2~%	4.5%	1.2~%	2.1%	1.6%	1.4~%	1.7 %	1.5%	1.6%
u	4506	1005	510	595	8060	1638	6252	4545	3510	2979	653	328	377	1693	331	1832	1312	1166	340	3283	491	2907	1243	662	620
θ	0.990	0.985	0.986	0.988	0.989	0.982	0.991	0.990	0.991	0.941	0.944	0.946	0.952	0.939	0.936	0.934	0.931	0.857	0.915	0.949	0.929	0.936	0.945	0.953	0.949
е	$0.118\mathrm{m}$	$0.148\mathrm{m}$	$0.169\mathrm{m}$	$0.135\mathrm{m}$	$0.132\mathrm{m}$	$0.166\mathrm{m}$	$0.117\mathrm{m}$	$0.125\mathrm{m}$	$0.124\mathrm{m}$	$0.860{ m m~s^{-1}}$	$0.827{ m m~s^{-1}}$	$0.800{ m m~s^{-1}}$	$0.807 { m m \ s^{-1}}$	$0.862{ m m~s^{-1}}$	$0.884{ m m~s^{-1}}$	$0.914{ m m~s^{-1}}$	$0.959{ m m~s^{-1}}$	$1.306{ m m~s^{-1}}$	$0.962{ m m~s^{-1}}$	$0.853{ m m~s^{-1}}$	$0.930{ m m~s^{-1}}$	$0.993{ m m~s^{-1}}$	$0.851{ m m~s^{-1}}$	$0.857{ m m~s^{-1}}$	$0.877{ m m~s^{-1}}$
e	$0.156\mathrm{m}$	$0.193\mathrm{m}$	$0.215\mathrm{m}$	$0.177\mathrm{m}$	$0.172\mathrm{m}$	$0.216\mathrm{m}$	$0.155\mathrm{m}$	$0.164\mathrm{m}$	$0.162\mathrm{m}$	$1.097{\rm m~s^{-1}}$	$1.056{ m m~s^{-1}}$	$1.056{ m m~s^{-1}}$	$1.040 {\rm m \ s^{-1}}$	$1.114{ m m~s^{-1}}$	$1.102{ m m~s^{-1}}$	$1.162{ m m~s^{-1}}$	$1.214{ m m~s^{-1}}$	$1.706{ m m~s^{-1}}$	$1.234{ m m~s^{-1}}$	$1.099 {\rm m~s^{-1}}$	$1.179 \mathrm{m~s^{-1}}$	$1.280{ m m~s^{-1}}$	$1.079{ m m~s^{-1}}$	$1.097{ m m~s^{-1}}$	$1.130{ m m~s^{-1}}$
Calibration Function	$H_s^* = 1.069 \cdot H_s - 0.201$	$H_{s}^{*} = 1.122 \cdot H_{s} + 0.255$	$H_s^* = 1.150 \cdot H_s + 0.366$	$H_s^* = 1.102 \cdot H_s + 0.273$	$H_s^* = 1.076 \cdot H_s + 0.042$	$H_s^* = 1.076 \cdot H_s + 0.122$	$H_s^* = 1.068 \cdot H_s + 0.102$	$H_s^{*} = 1.036 \cdot H_s + 0.026$	$H_s^* = 1.050 \cdot H_s - 0.088$	$U_{10}^* = 1.010 \cdot U_{10} - 0.110$	$U_{10}^{*} = 1.066 \cdot U_{10} - 0.395$	$U_{10}^{*} = 1.025 \cdot U_{10} + 0.128$	$U_{10}^{*} = 1.046 \cdot U_{10} - 0.562$	$U_{10}^{*} = 1.043 \cdot U_{10} - 0.071$	$U_{10}^{*} = 0.980 \cdot U_{10} - 0.119$	$U_{10}^{*} = 0.972 \cdot U_{10} - 0.036$	$U_{10}^{*} = 1.041 \cdot U_{10} - 0.101$	$U_{10}^{*} = 1.015 \cdot U_{10} - 0.087$	$U_{10}^{*} = 0.976 \cdot U_{10} - 0.623$	$U_{10}^{*} = 1.015 \cdot U_{10} + 0.033$	$U_{10}^{*} = 0.903 \cdot U_{10} - 0.489$	$U_{10}^{*} = 0.999 \cdot U_{10} + 0.070$	$U_{10}^{*} = 0.991 \cdot U_{10} + 0.003$	$U_{10}^* = 1.031 \cdot U_{10} - 0.140$	$U_{10}^{*} = 1.018 \cdot U_{10} - 0.050$
Scope	24 September 2002 – 17 November 2008	01 August 1991 – 01 January 1994	01 January 1994 – 18 April 1995	18 April 1995 – 02 June 1996	29 April 1995 - 08 September 2008	31 March 1985 – 30 December 1989	07 January 2000 – 01 July 2008	15 January 2002 – 03 May 2008	25 September $1992 - 08$ October 2005	24 September $2002 - 17$ November 2008	01 August 1991 – 01 January 1994	01 January 1994 – 18 April 1995	18 April 1995 – 02 June 1996	29 April 1995 – 12 February 2000	12 February 2000 – 10 February 2001	10 February 2001 – 24 May 2005	24 May 2005 – 08 September 2008	31 April 1985 – 30 December 1989	07 January $2000 - 21$ December 2000	21 December 2000 - 21 January 2007	21 January 2007 – 01 July 2008	15 January 2002 – 03 May 2008	22 September 1992 – 10 February 2001	10 February 2001 – 21 October 2003	21 October 2003 – 08 October 2005
Altimeter	ENVISAT	ERS1	ERS1	ERS1	ERS2	GEOSAT	GFO	JASON1	TOPEX	ENVISAT	ERS1	ERS1	ERS1	ERS2	ERS2	ERS2	ERS2	GEOSAT	GFO	GFO	GFO	JASON1	TOPEX	TOPEX	TOPEX
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FIG. 1. Global distribution of all 195 NODC buoy stations distributed over 619 different locations based on a Mollweide interrupted equal-area projection. The spatial coverage is clearly limited to the Northern Hemisphere, whilst the temporal coverage features hourly records since 1985.



FIG. 2. Temporal coverage of available datasets of the previous seven altimeter missions.



FIG. 3. Ascending GFO ground track recorded on 5 September 2007 (cycle 201, pass 34) commencing over the Antarctica and proceeding over the Southern Ocean, North Pacific Ocean towards the Arctic Ocean (left panel). The right panels show H_s and U_{10} as a function of latitude recorded along the ground track. Data errors ("spikes") are clearly evident in the data. This erroneous data (shown in gray) has been removed by the quality control process.



FIG. 4. Calibration results for JASON1 altimeter data. Shaded scatter density plot for significant wave height (upper) and wind speed (lower graph) of collocated measurements are shown. Collocated measurements are considered within 50 km radius and 30 min temporal separation. Error statistics for RMSE (ϵ), correlation coefficient (ρ), number (n) of sample point are given with outliers (n_{out}) labeled with crosses. The solid line represents the RMA fit. The axes were divided into 40 even increments and the contours show the number of data points in each increment square.



FIG. 5. Comparison of proposed wind speed algorithms for the estimation of wind speed, U_{10} from the altimeter radar backscatter (σ_o). The shaded contour plot shows isolines of data point density. The axes were each divided into 40 equally sized bins and the number of data points in each bin determined. Data is shown for TOPEX normalized radar cross section, σ_o adjusted by -0.502 dB. Note that with the exception of Young (1993), algorithms have been developed with data less than $U_{10} \approx 20 \, m \, s^{-1}$. The results have been extrapolated beyond this value to show the effect of extrapolation to such wind speeds.



FIG. 6. Distribution of co-located measurements between JASON1 and ERS2 radar altimeters. During the latter part of the ERS2 mission an on-board storage failure limited the spatial coverage to the Northern Hemisphere. As a result, there is a greater density of co-location points in the North Atlantic and parts of the North Pacific.



FIG. 7. Collocated measurements between JASON1 and ERS2 altimeters. Shaded scatter density plots show significant wave height (upper) and wind speed (lower graph). Contours are calculated as in Figure 4.



FIG. 8. Plot (20/1 block averages) illustrating differences in significant wave height between uncalibrated TOPEX and calibrated ERS2 measurements. The proposed drift correction f(t)(Eq. (8)) with t in days was applied between 25 April 1997 and 30 January 1999, equivalent to cycles 170 to 235. Dash-dotted lines represent 1/2 standard deviation boundaries. The time period of the drift is shown by the shaded region. The white dots in this region shows the altimeter differences once the TOPEX drift has been removed using Eq. (8).



FIG. 9. Differences in H_s between TOPEX and buoy observations after applying the drift correction (Eq. (8)) and calibration function (cf. Table 4). The plot (block averaged at 12/1) covers the same time span as in Figure 8.



FIG. 10. Plot (block averaged at 12/1) showing differences between ERS1 and buoy H_s and U_{10} . The shaded region shows a time-dependent offset in H_s . The panels to the right show the differences once the partial RMA analysis was performed, removing the offset. Error statistics prior to the partial RMA analysis are: $\epsilon_{H_s}=0.20 \text{ m}$, $\epsilon_{U_{10}}=1.11 \text{ m s}^{-1}$. The partial RMA analysis reduces these values to: $\epsilon_{H_s}=0.19 \text{ m}$ and $\epsilon_{U_{10}}=1.10 \text{ m s}^{-1}$.



FIG. 11. Differences between GFO and buoy H_s and U_{10} . Deviations (shaded areas) in GFO wind speed measurements were successfully removed using the partial RMA calibration approach. Wind speed rms errors were improved from $\epsilon_{U_{10}}=1.20 \text{ m s}^{-1}$ (left) to $\epsilon_{U_{10}}=1.18 \text{ m s}^{-1}$ (right) while significant wave height was not altered $\epsilon_{H_s}=0.15 \text{ m}$.