Three - Dimensionnal coupled modeling of wave- and wind/buoyancy- driven currents Example from the Gulf of Aigues - Mortes (NW Mediterranean sea, France)

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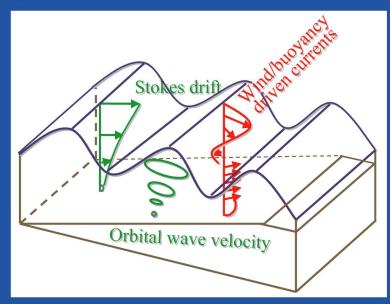








Rationale



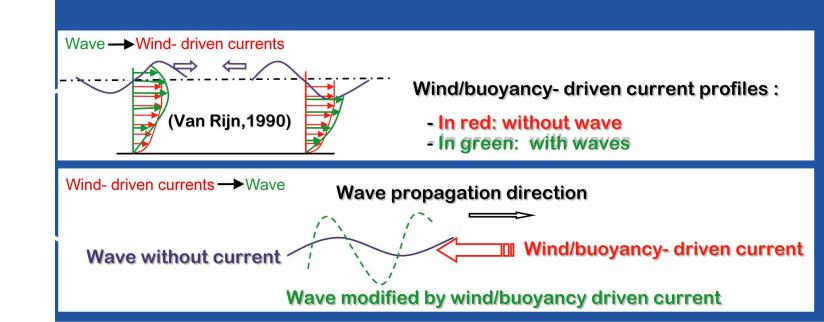
Hydrodynamics of nearshore tidalless continental shelf depends on two main processes:

- wind/buoyancy- driven currents
- wave-driven currents

Simulations on the Gulf of Aigues-Mortes (GAM, NW Mediterranean sea, France), a prototypic area, show that these two types of currents:

- present strong vertical variations in intensity and/or direction
- have an intensity of the same order of magnitude
 - interract

It is thus necessary to take into account the **two** processes as well as their **three-dimensionnal** coupled effects.

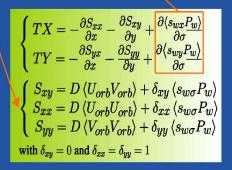


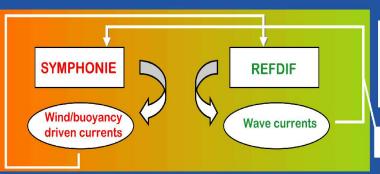
Coupling of the circulation model SYMPHONIE and the wave model REF/DIF

The **SYMPHONIE** model, adapted from the Johns *et al.* (1991) model, has been developed for ten years by the Laboratoire d'Aerologie (Toulouse, France) and is now largely used by the French community to compute the **oceanic circulation** on continental shelves, and specically on the Gulf of Lion. This model is based on the **three-dimensional primitive equations** and is widely described in Estournel et al. (1997). The coupling of SYMPHONIE with the REFDIF model allows to impose the **wave driving terms**, TX and TY, as forcing in the **Navier-Stokes equations**. These terms are composed of the **radiation stress** gradients and the wave **overpressure terms**.

REF/DIF is a weakly non linear combined refraction and diffraction model based on the parabolized "mild-slope equation" (Berkhoff equation, 1972) and the Mei and Tuck parabolic diffraction model (1980). This model takes into account the influence of a Doppler velocity which is usually a vertically integrated general current (Booij, 1981; Kirby, 1984).

The coupled wind- and wave- driven currents model allows to include the "Doppler velocity" UD from Symphonie model, through Kirby and Chen (1989).





$$\begin{cases} U_{Dx}(x,y) = \int_0^1 u_{cx}(x,y,\sigma) \frac{kD \cosh(2kD\sigma)}{\sinh(2kD)} d\sigma \\ U_{Dy}(x,y) = \int_0^1 u_{cy}(x,y,\sigma) \frac{kD \cosh(2kD\sigma)}{\sinh(2kD)} d\sigma \end{cases}$$

Described in this poster

The equations of motion are those given by Mellor (2003) and Denamiel (2003):

$$\begin{split} & \cdot \frac{\partial DU*}{\partial x} + \frac{\partial DV*}{\partial y} + \frac{\partial \Omega}{\partial \sigma} + \frac{\partial \zeta_c}{\partial t} = 0 \\ & \cdot \left\{ \begin{array}{l} \frac{\partial DU*}{\partial t} + \frac{\partial DU*U*}{\partial x} + \frac{\partial DU*V*}{\partial y} + \frac{\partial (\Omega U*)}{\partial \sigma} - fDV* + \frac{\partial DP_c}{\partial x} - \frac{\partial}{\partial \sigma} (\sigma \frac{\partial D}{\partial x} P_c) + gD \frac{\zeta_c}{\partial x} = TX - \frac{\partial w' \overline{u'}}{\partial \sigma} \\ \frac{\partial DV*}{\partial t} + \frac{\partial DV*U*}{\partial x} + \frac{\partial DV*V*}{\partial y} + \frac{\partial (\Omega V*)}{\partial \sigma} + fDU* + \frac{\partial DP_c}{\partial y} - \frac{\partial}{\partial \sigma} (\sigma \frac{\partial D}{\partial y} P_c) + gD \frac{\zeta_c}{\partial y} = TY - \frac{\partial w' \overline{v'}}{\partial \sigma} \\ \frac{\partial P_c}{\partial \sigma} = -Dg \frac{\rho_c}{\rho_0} \end{split}$$

where $\bullet \langle \rangle = \frac{1}{2\pi} \int_0^{2\pi} ()d\psi$ is the wave phase averaging operator with $\psi = \sigma t - \overrightarrow{k} \overrightarrow{x}$ the wave phase

- $s(x,y,\sigma,t)=\sigma D-h+s_w$ is the sigma vertical coordinate with $D=h+\zeta_c$ the mean water column depth, h(x,y) the bottom depth, $\zeta_c(x,y)$ the mean elevation due to wind and buoyancy forcing and $s_w(x,y,\sigma,t)=a\frac{\sinh(k)D\sigma}{\sinh(k)D}\cos\psi$ is the instantaneous elevation due to wave
- $\overrightarrow{U*} = (U*, V*, \Omega) \text{ is the total current} : \overrightarrow{U*} = \overrightarrow{U_{stokes}} + \overrightarrow{u_c} \text{ and } \overrightarrow{U_{stokes}}, V_{stokes}) = \begin{cases} U_{stokes} = \frac{(ak)^2}{2} C \cos\theta \frac{\cosh(2kh\sigma)}{2} \cos(2kh\sigma) \\ V_{stokes} = \frac{(ak)^2}{2} C \sin\theta \frac{\cosh(2kh\sigma)}{2} \cos(2kh\sigma) \\ V_{stokes} = \frac{(ak)^2}{2} C \sin\theta \frac{\cosh(2kh\sigma)}{2} \cos(2kh\sigma) \end{cases}$
- k is the wave number, C is the intrinsic phase speed $(C^2 = \frac{a}{k} tanh(kh + \frac{a}{kh}))$ and a is the wave amplitude
- $P = P_w + P_c$ is the total pressure with $P_w + gz = ga\frac{\cosh(kh\sigma)}{\cosh(kh\sigma)}cos(\psi)$ the wave pressure and P_c the hydrostatic pressure
- w'u' and w'v' are the Reynolds stresses
- $\overrightarrow{u_r(x,y,\sigma)}$ is the wind/buoyancy- driven velocity

Academic case study

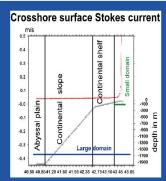
This study presents the introduction of the wave forcing terms into the SYMPHONIE model on linear and regular bathymetry. In order to optimize computations, a grid nesting was realized with a large domain including an abyssal plain from 2000 m water depth, a continental 1% slope and a 0.2% continental shelf.

The wave conditions were supposed to be constant except on the small domain (h > -70 m)

These conditions are:

- · first order and monochromatic Stokes wave
- amplitude: 2m
- period: 10s
- direction: southern towards northern

On the small domain, the wave propagation is computed thanks to the REF/DIF model. The results are then interpolated and introduced into the SYMPHONIE model in form TX, TY and the circulation model is initialized with the Stokes currents.



Caution:

- periodic conditions are imposed on the eastern and western boundaries of the domains
- water height conservation conditions are imposed on the offshore open boundary

Z- profile of Z- profile of Z- profile of crosshore velocities crosshore velocities rosshore velocities -800 m depth -80 m depth -25 m depth velocity (m/s) velocity (m/s) 10 -0.05 -0.00 0.05 0.10 0.15 0.20 0.25 0.30 0.35 -0.3 -0.2 -0.1 0.0 0.1 0.2 0.3 depth in m Z- profile of crosshore velocities gitudinal Profile -2000 m depth velocity (m/s)

Duration of simulation: 17 hours

In the particular case of a linear and regular bathymetry the study of one longitudinal profile is sufficient.

Southern wind only (black feature): pilot simulation showing classical results obtained without wave interaction

Southern wave intialization without wave forcing terms (brown feature): the final state fall at rest. Indeed, after the domain initialization, there is not any more forcing (wave nor wind).

1) sea surface elevation:

m/s

- h < -20 m: the elevation is equal to 0 cm.
- -10 m < h < -5 m: set-down which reaches -10 cm for the southern wave simulation (red feature). It increases up to -5 cm with a southern wind (green feature) and decreases up to -18 cm with a northen wind (blue feature).
- h > -5 m: set-up which reaches + 60 cm for the southern wave simulation (red feature). It increases up to + 70 cm with a southern wind (green feature) and remains identical with a northen wind (blue feature).
- 2) transports: mainly eastward longshore transports (longshore transports mean intensity: 2 m²/s and crosshore transports mean intensity: 0.10 m²/s)
- h < $65\ m$: transports decrease for all the simulations because of the offshore boundary condition
- - 65 m < h < 30 m : longshore transports increase and reach 2.8 m^2/s for the southern wave simulation (red feature), 3.0 m^2/s with a southern wind (green feature) and 2.3 m^2/s with a northen wind (blue feature)
- h > -5 m: " the wave sees the bottom" and the transports deacrease to 0 m²/s

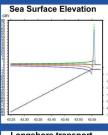
 3) bottom currents: mainly southtward crosshore currents (longshore currents mean intensity: 0.02 m/s and crosshore currents mean intensity: 0.3 m/s)

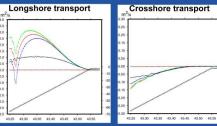
4) surface currents: mainly northwards crosshore currents (longshore currents mean intensity: 0.05 m/s) and crosshore currents mean intensity: 0.05 m/s and crosshore currents mean intensity: 0.3 m/s)

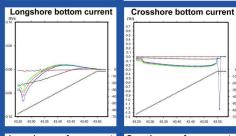
This two currents have the same behaviour and intensities and compensate themselves:

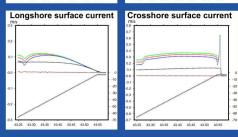
- h < 65 m: crosshore currents decrease for all the simulations because of the offshore boundary condition
- - 65 m < h < 5 m: crosshore currents remains relatively constant to 0.28 m/s for the southern wave simulation (red feature), 0.3 m/s with a southern wind (green feature) and 0.25 m/s with a northen wind (blue feature)
 - h > -5 m: surface and bottom currents increase respectively up to 0.6 m/s and to 1.3

Longitudinal Profiles on the small domain











Southern waves and wind
Southern waves and northern wind

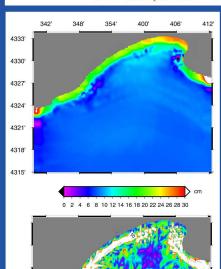
. Waves without wave forcing terms and wind Southern wind without waves

5) z- profiles: highlight the current direction shear

- offshore: 2000 m and 800 m depth
- 1- The inversion occurs on a 300 m thickness.
- 2- Contrary to other simulations, the surface current with a northern wind is directed northward.
 - on the small domain: 70 m and 25 m depth
- 1- The inversion occurs between the **surface** and the **bottom**.
 2- Bottom currents **increase** when the wave "sees the bottom".

Application to the gulf of Aigues-Mortes

Southern wave condition: 2 m amplitude and 10 s period



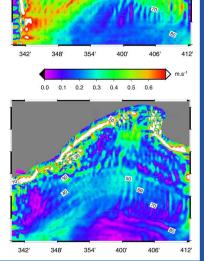
Sea surface elevation:

it is similar to the academic

- · Offshore: the elevation remains constant and is about +10 cm
- -20 m < h < -15 m, it decreases up to 4 cm
- h > -5 m, it strongly increases and reaches +20

Surface currents:

- offshore: the velocities are about 0.15 m/s and directed northward.
- -60 m < h < -30 m : they increase strongly and reach 0.6 m/s.
- h > -5 m: they strongly increase : > 0.6 m/s and they become longshore velocities.



Bottom currents:

- offshore: the velocities are about 0.05 m/s and directed southward.
- -60 m < h < -30 m: they increase and reach 0.3 m/s.
- h > -5 m: they strongly increase: > 0.6 m/s and they become longshore velocities In this area there are two nearshore drifts.

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